

Modellierung und Korrektur dynamischer elektrischer Wellenformen

23NRM01 SBS Uncert

Support for standardization of sample-by-sample waveform uncertainty calculation

333. PTB Seminar, 06.05.2026

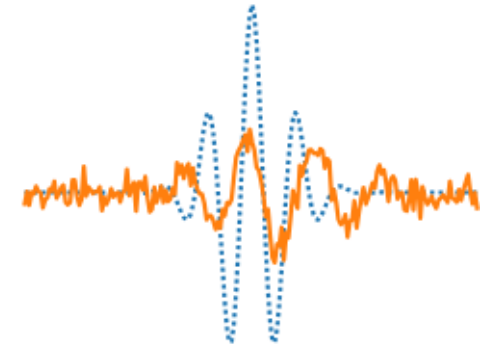
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Outline

- Motivation
- Digital Sampling Oscilloscopes
- Digital Real-Time Oscilloscopes

Motivation

- Knowledge of exact waveform of growing importance
 - High-bandwidth communication technology
 - Electrical power grid stability
- Significant influence of measurement system
 - Device impairments need to be characterized
 - Measured waveforms need to be corrected
- Adaption of existing knowledge (GUM, ...) not always straight-forward
 - Sample-by-sample uncertainty computation



IEC: Sample-by-sample waveform uncertainty computation

Support the writing of a new IEC standard

- IEC Working title
Electrical Waveform Uncertainties
- Complements existing standard IEC 62754
*Computation of waveform **parameter** uncertainties*
- New standard: **waveform metrology**
 - waveform reconstruction and processing methods
 - uncertainty analysis/propagation methods

INTERNATIONAL
STANDARD

NORME
INTERNATIONALE



Computation of waveform parameter uncertainties

Calcul des incertitudes des paramètres des formes d'onde

<https://webstore.iec.ch/en/publication/29773>

IEC: Sample-by-sample waveform uncertainty computation

IEC 62754:

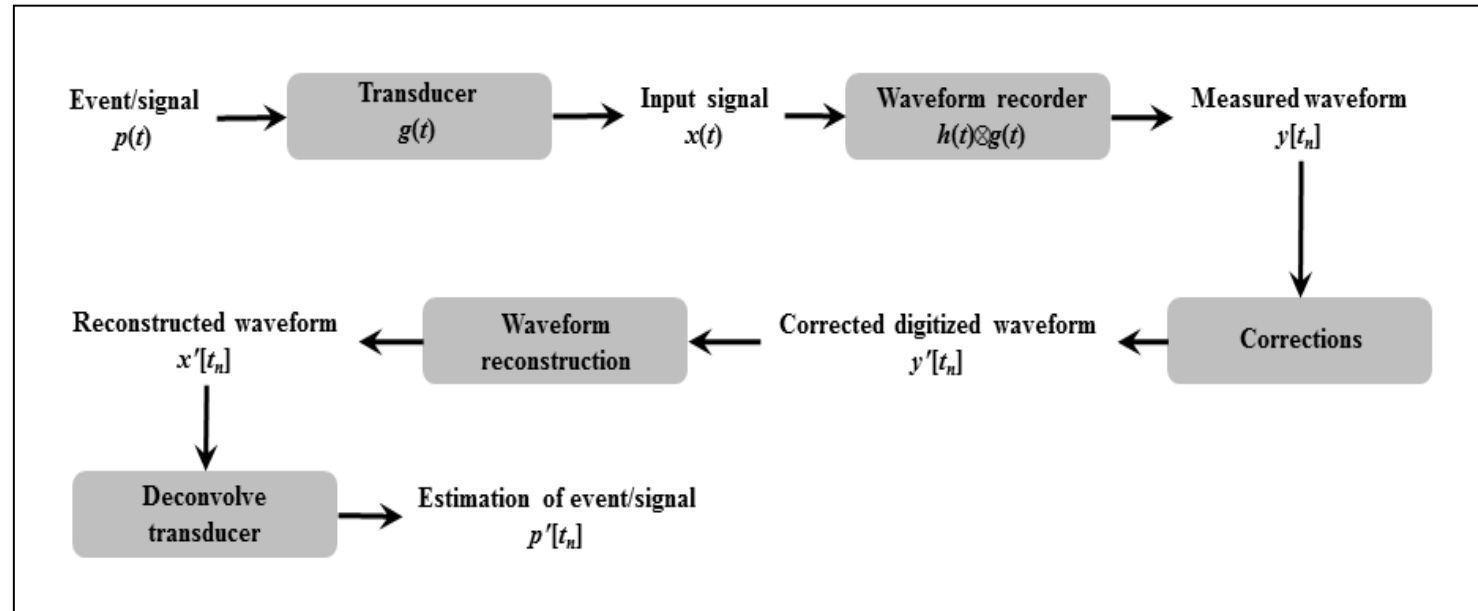
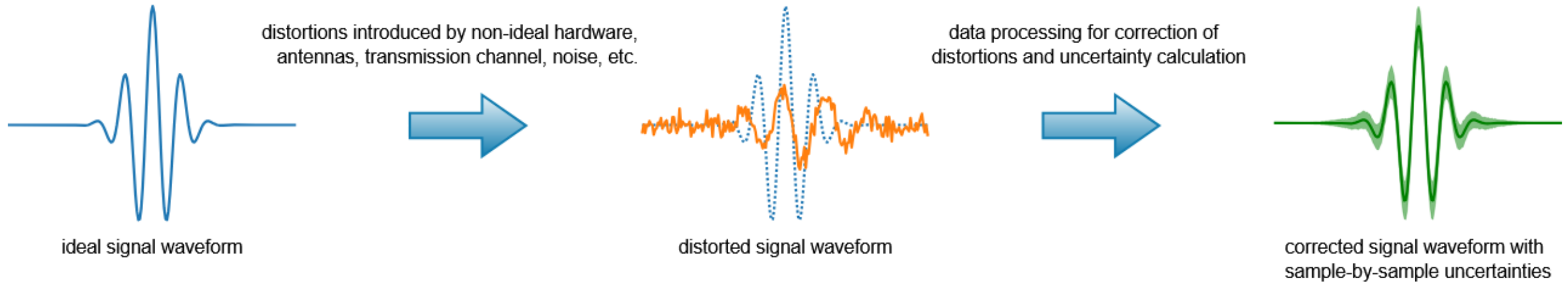


Figure 3 – Creation of measured, corrected, and reconstructed waveforms and the final estimate of the input signal

5.3.2 Sample-by-sample correction

Sample-by-sample waveform corrections and their resultant contribution to both sample-by-sample waveform uncertainties and waveform parameter uncertainties **will be the subject of a different documentary standard** but a brief mention is provided in 5.3.2.

EURAMET 23NRM01: SBS Uncert



Selected instruments

- sampling oscilloscopes
- real-time digital oscilloscopes
- ~~ADCs~~

not today

Tasks

1. system modelling
2. characterization of impairments
3. waveform correction / reconstruction
4. uncertainty propagation

Outline

- Motivation
- Digital Sampling Oscilloscopes
- Digital Real-Time Oscilloscopes

Digital Sampling Oscilloscopes

- High bandwidth (up to 110 GHz bandwidth)
- Cost efficient per GHz: fraction of price of real-time oscilloscopes
- Use cases:
 - Analysis of high-speed data transmission signals
 - Compliance testing, TDR measurements
- Advantages:
 - High resolution, low noise, minimal jitter
 - Established technique (characterization, data correction)
- Limits:
 - Repetitive signals only
 - Trigger dependency
 - Distortions due to hardware imperfections

DSO: Model



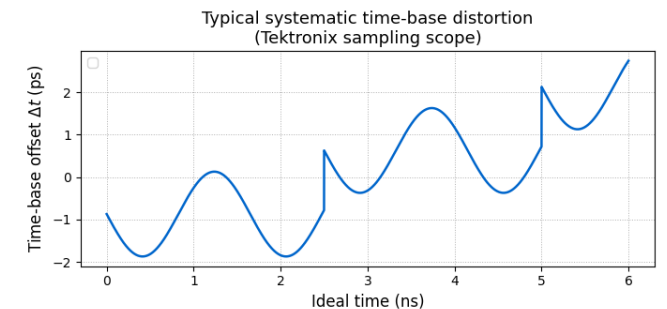
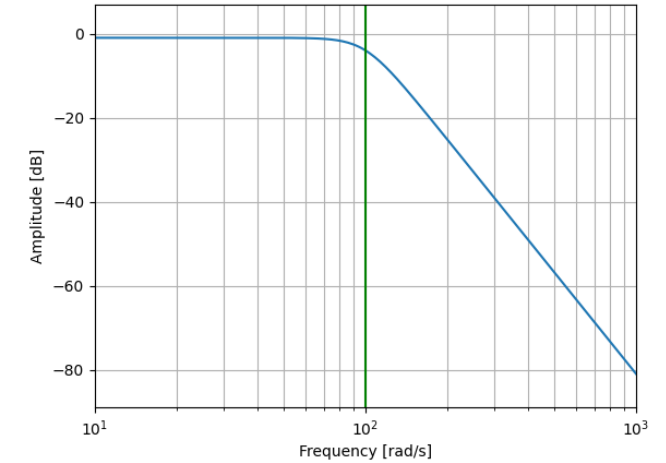
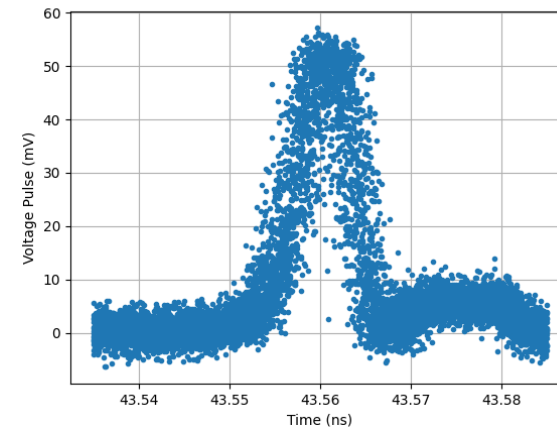
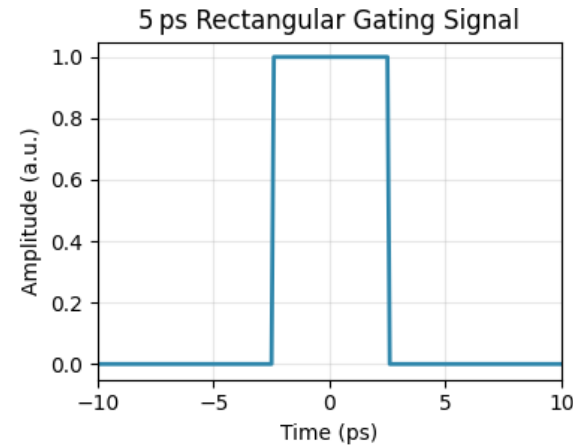
- Time gating (sample-and-hold)
- Low-pass filter
- White-noise jitter
- Connector losses, mismatch

front
end

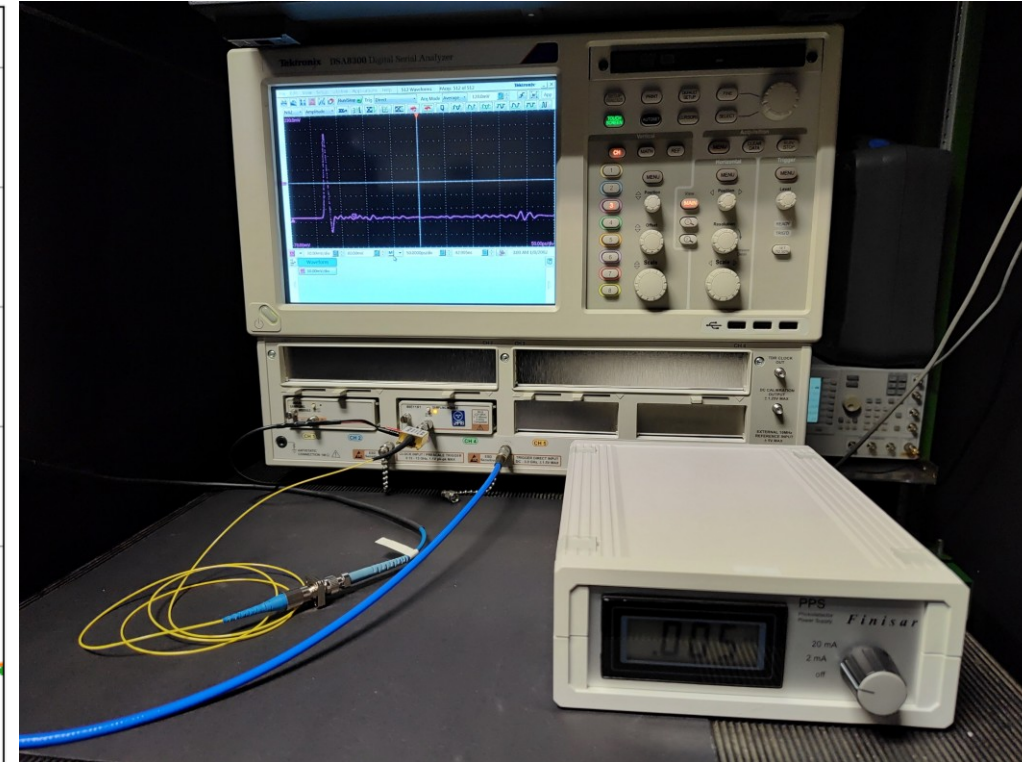
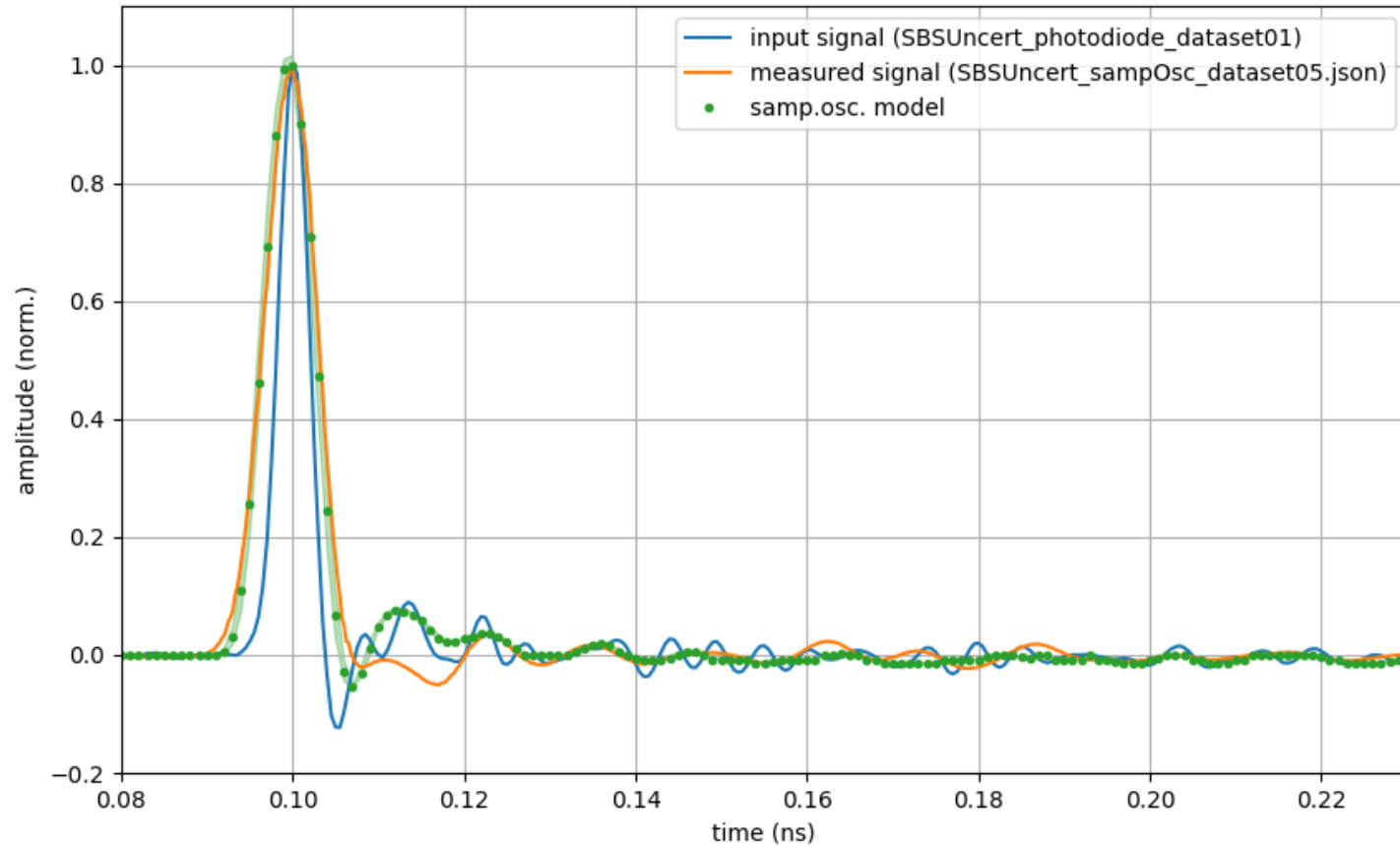
- Systematic time base distortion
- Interpolate sampling instants
- Quantisation errors

ADC

→ Set up transfer function $H(f)$
→ Apply to data $H(f) \cdot X(f) = Y(f)$



DSO: Model vs. Measurements



DSO: Waveform correction

Recipe

1. model a transfer function $H(f)$
2. model an input signal $x(t)$
3. ,measure' by applying H :

$$H(f) \cdot X(f) = Y(f) \rightarrow y(t)$$
4. Reconstruct via deconvolution

$$X_{\text{recon}}(f) = Y(f) / H(f) \rightarrow x_{\text{recon}}(t)$$

→ What about the uncertainty?

→ **Correlation is key!**

Mean and standard deviation

amplitude: $0.9966 \text{ V} \pm 0.0039 \text{ V}$ ($k=2$)

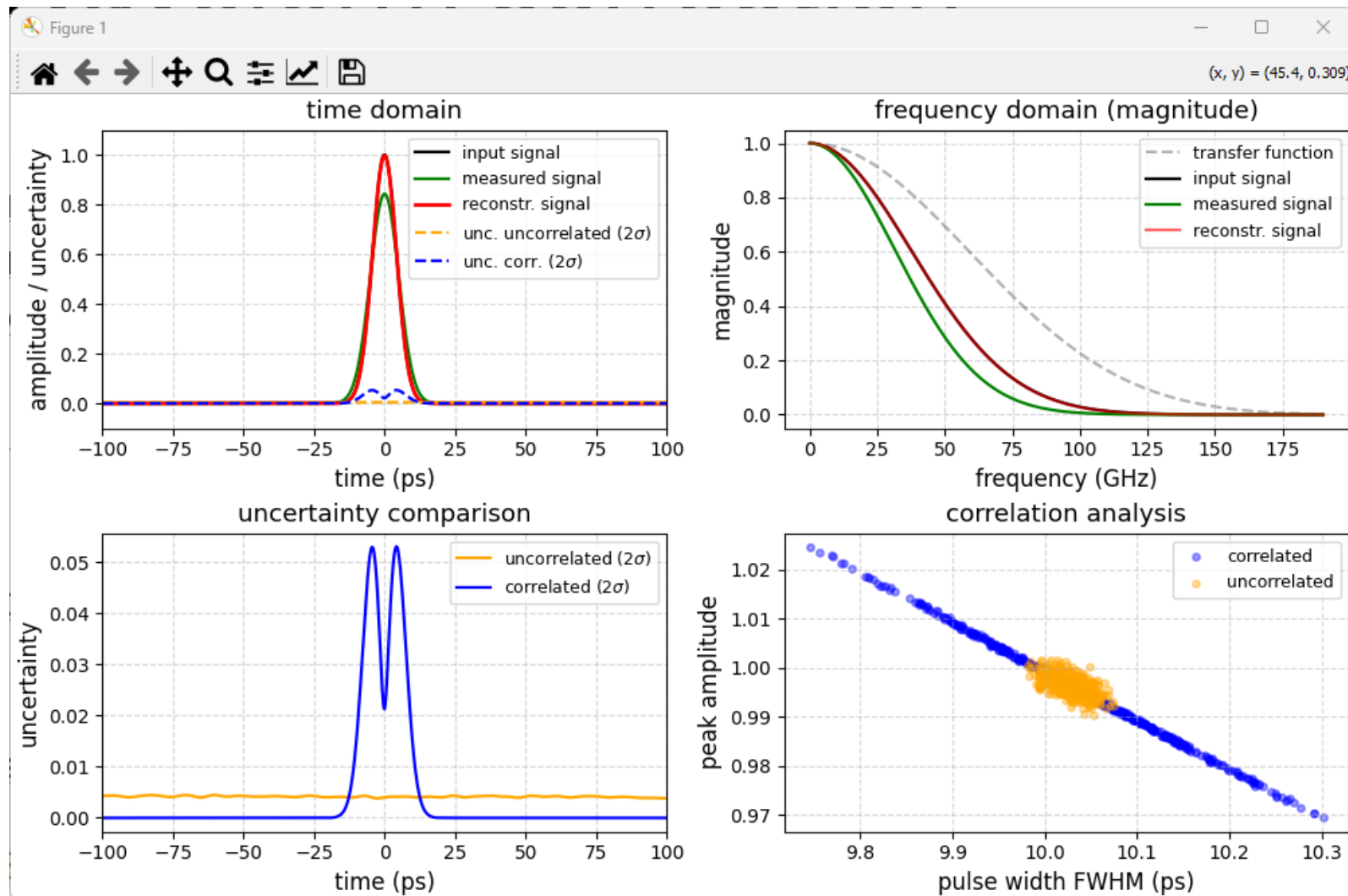
FWHM: $10.03 \text{ ps} \pm 0.03 \text{ ps}$ ($k=2$)

Mean and covariance matrix

amplitude: $0.9957 \text{ V} \pm 0.0211 \text{ V}$ ($k=2$)

FWHM: $10.03 \text{ ps} \pm 0.21 \text{ ps}$ ($k=2$)

$r(A, \text{FWHM})$: -0.9997



DSO: Waveform correction

Recipe

1. model a transfer function $H(f)$
2. model an input signal $x(t)$
3. ,measure' by applying H :
 $H(f) \cdot X(f) = Y(f) \rightarrow y(t)$
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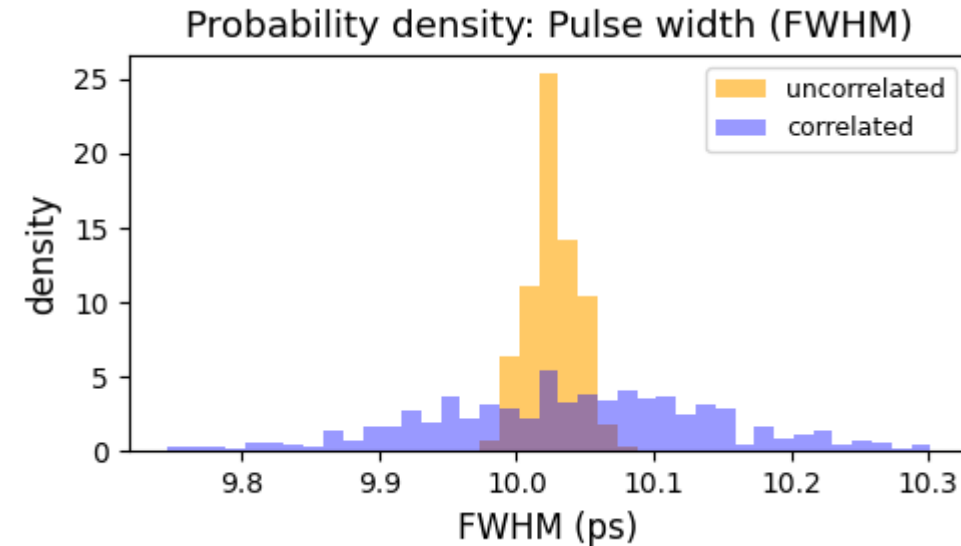
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Mean and covariance matrix

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FWHM: $10.03 \text{ ps} \pm 0.21 \text{ ps}$ ($k=2$)

$r(A, \text{FWHM})$: -0.9997



Waveform correction w/o covariance matrix

- Underestimates the uncertainty
- Hides correlations
- May introduce statistical bias

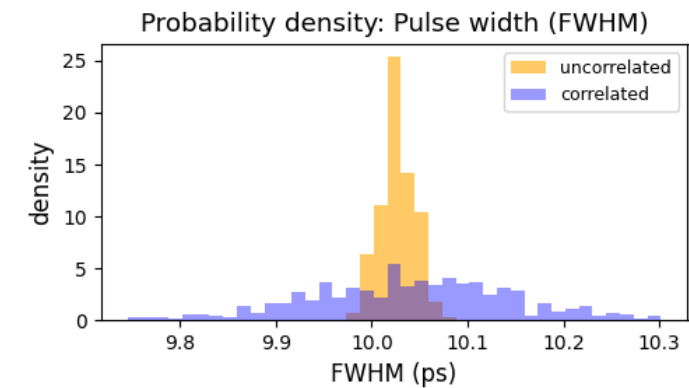
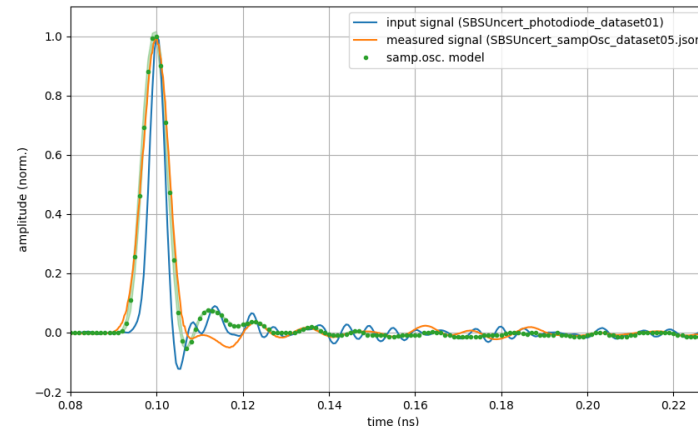
DSO: Summary

DSO Model

- Impairments due to front end + ADC
 - Parameter tuning to match different oscilloscopes
- Input signal via
 - measurement data
 - source models (photodiode, electrical pulse generator)
- model output matches measurements

Waveform Correction

- Based on model transfer function
- Includes sample-by-sample waveform uncertainty computation
- Highlights relevance of covariance matrix for signal reconstruction

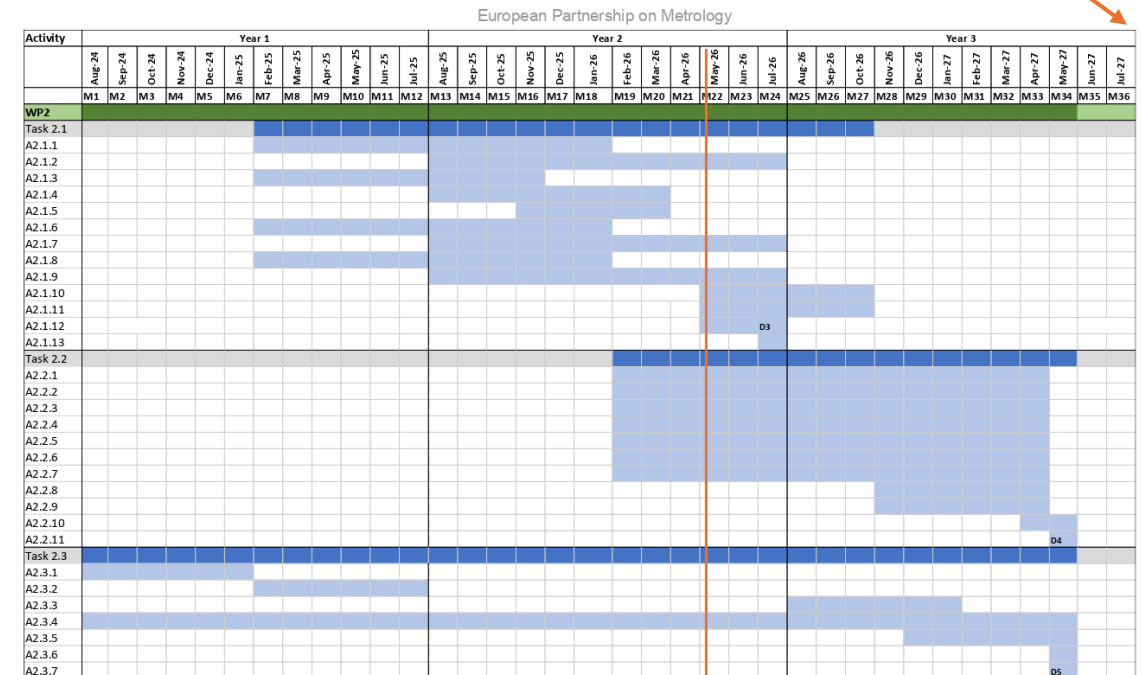


DSO: Next steps

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- Model validation / improvement
 - Different architectures, input sources
- Implement efficient calculation methods
 - Advanced Monte Carlo Methods
 - Principle Component Analysis
- Contribute to IEC standard
- Online-services for easy-access to model and reconstruction routines
 - International Data Spaces („QI-Digital“)
 - „correct your data online“ (DCC, ...)

08/2027



Outline

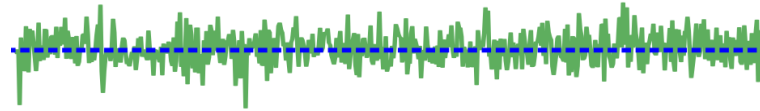
- Motivation
- Digital Sampling Oscilloscopes
- Digital Real-Time Oscilloscopes

Digital Real-Time Oscilloscopes

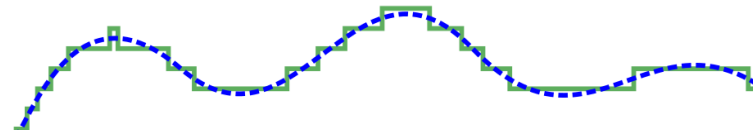
- Broadband instruments (up to 110 GHz bandwidth, 256 GS/s)
- Relatively cost efficient
- Use cases:
 - Demodulation of optical communication signals
 - Broadband signal integrity measurement
- Advantages:
 - Sophisticated signal post-processing available
 - Real-time measurement
- Limits:
 - Fast ADC architecture limits vertical resolution
 - Low dynamic range
 - Distortions due to hardware imperfections

Impairments of fast DRTOS

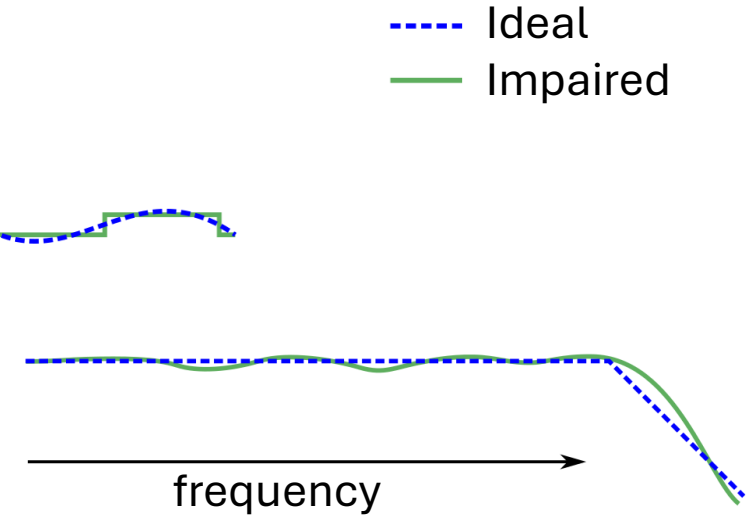
- Noise



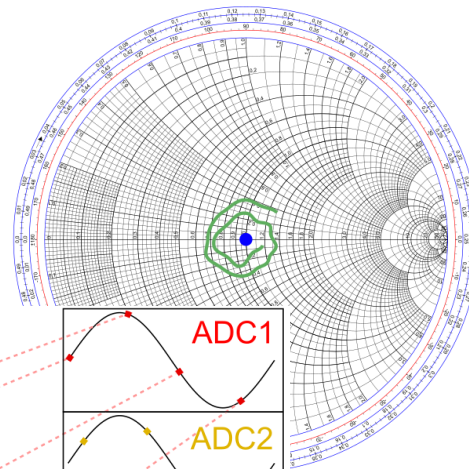
- Quantization



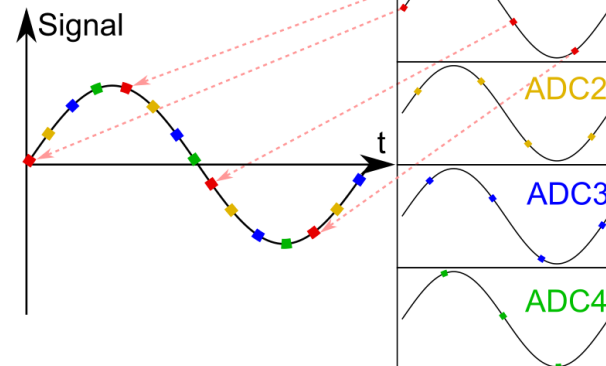
- Flatness / frequency response



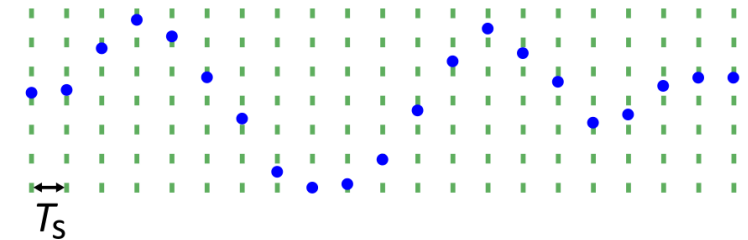
- Impedance mismatch



- Time-base stability



- Interleaving error

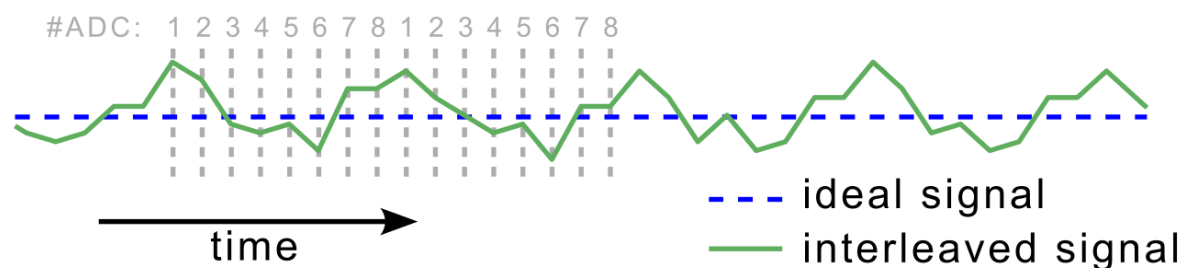


Interleaving Errors – why they matter

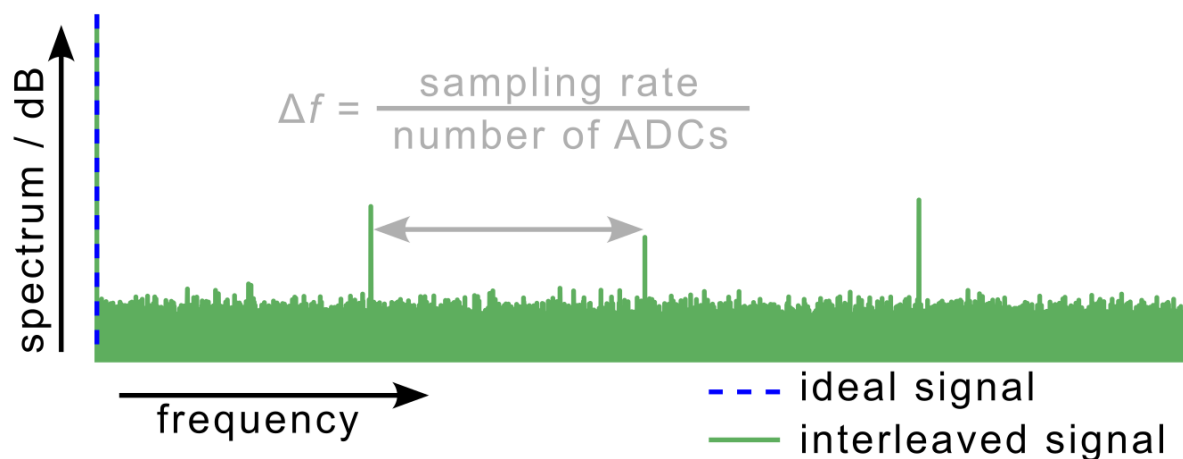
The synthesis of one fast signal from several sub-ADCs

- leads to a **repetitive pattern** in time domain.

Example with 8 sub-ADCs:



- corresponds to **sharp spurs** in frequency domain

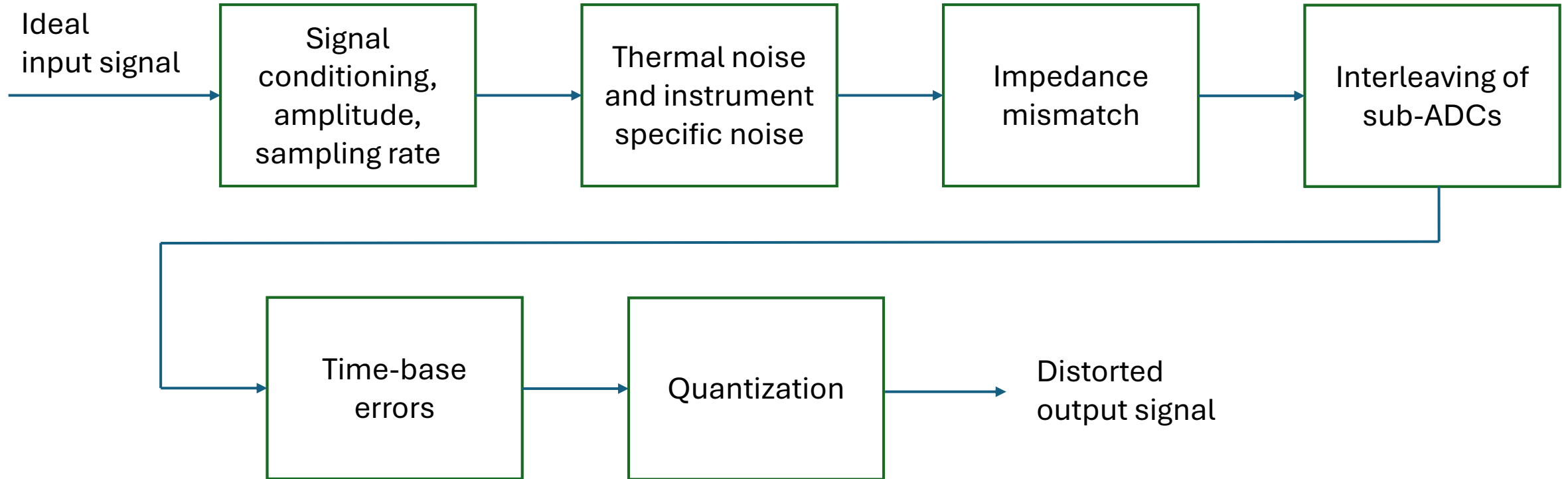


Issue:

Some input signal signals are affected more than others!

Examples: Sine at Δf ,
broadband pulses

Modeling of DRT0 Impairments



Characterization of Interleaving Error

Step 1:

- Finding the number of ADCs from noise measurement
 - Number of ADCs = sampling rate / Δf between spurs

Step 2:

- Characterizing the properties of sub-ADCs

Two published methods:

Relative difference between sub-ADCs¹

- Can remove interleaving spurs
- Simple measurement setup

Absolute transfer function of sub-ADCs²

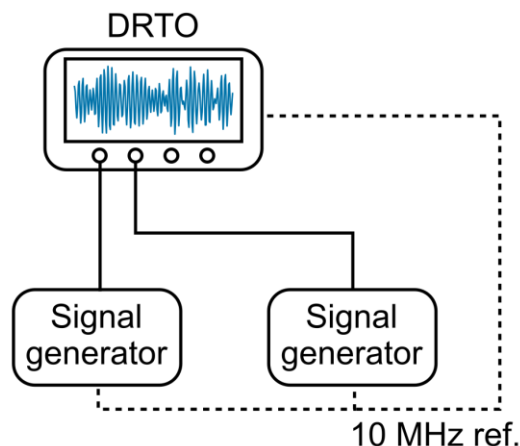
- Remove interleaving spurs
- Complex measurement setup

[1] C. Cho et al., "Calibration of Time-Interleaved Errors in Digital Real-Time Oscilloscopes," IEEE Trans. Microw. Theory Techn., vol. 64, no. 11, 2016.

[2] D. Kim et al., "Traceable calibration for a digital real-time oscilloscope with time interleaving architecture," Measurement Science and Technology, vol. 29, no. 1, 2018.

Relative Transfer Functions

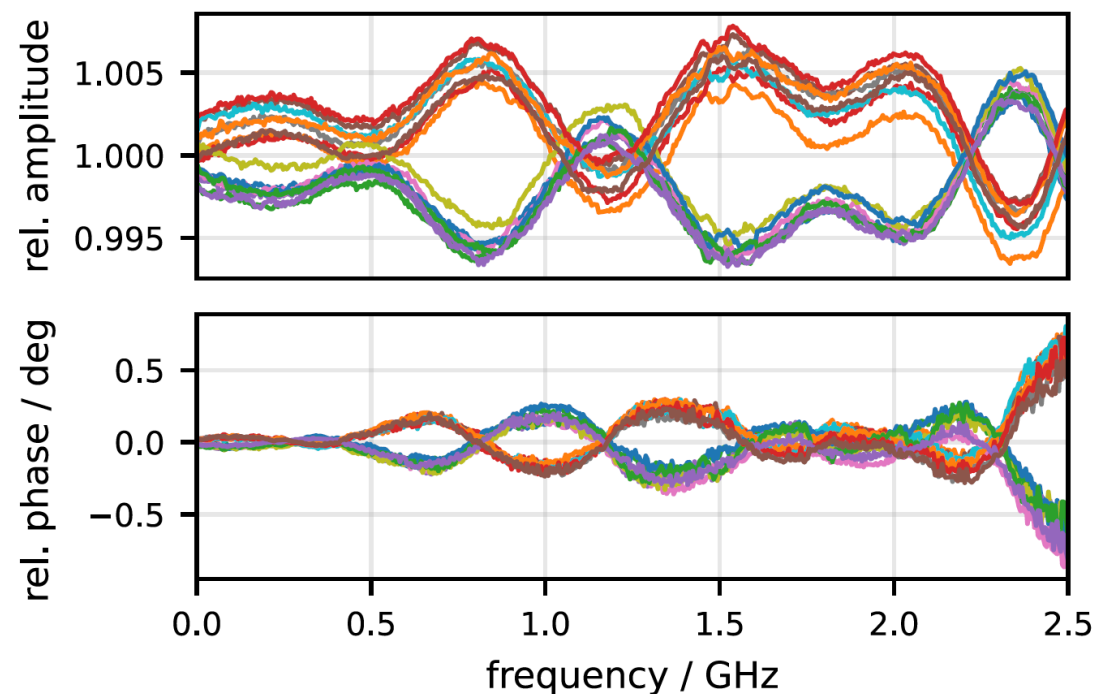
Setup



Main steps

- Port 1: swept sine, Port 3: reference sine
- Separate data by sub-ADCs
- Perform least-squares fit for each sub-ADC to find relative transfer function
- Assemble frequency dependent, relative transfer functions

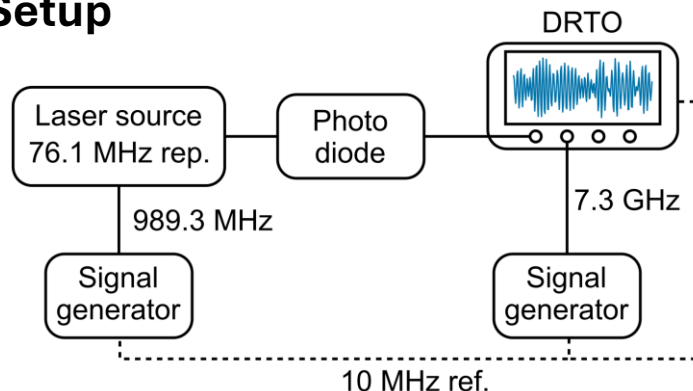
Exemplary results:



Relative transfer functions of 16 sub-ADCs from a DRT0 with 2.5 GHz Bandwidth, 20 GS/s sampling rate

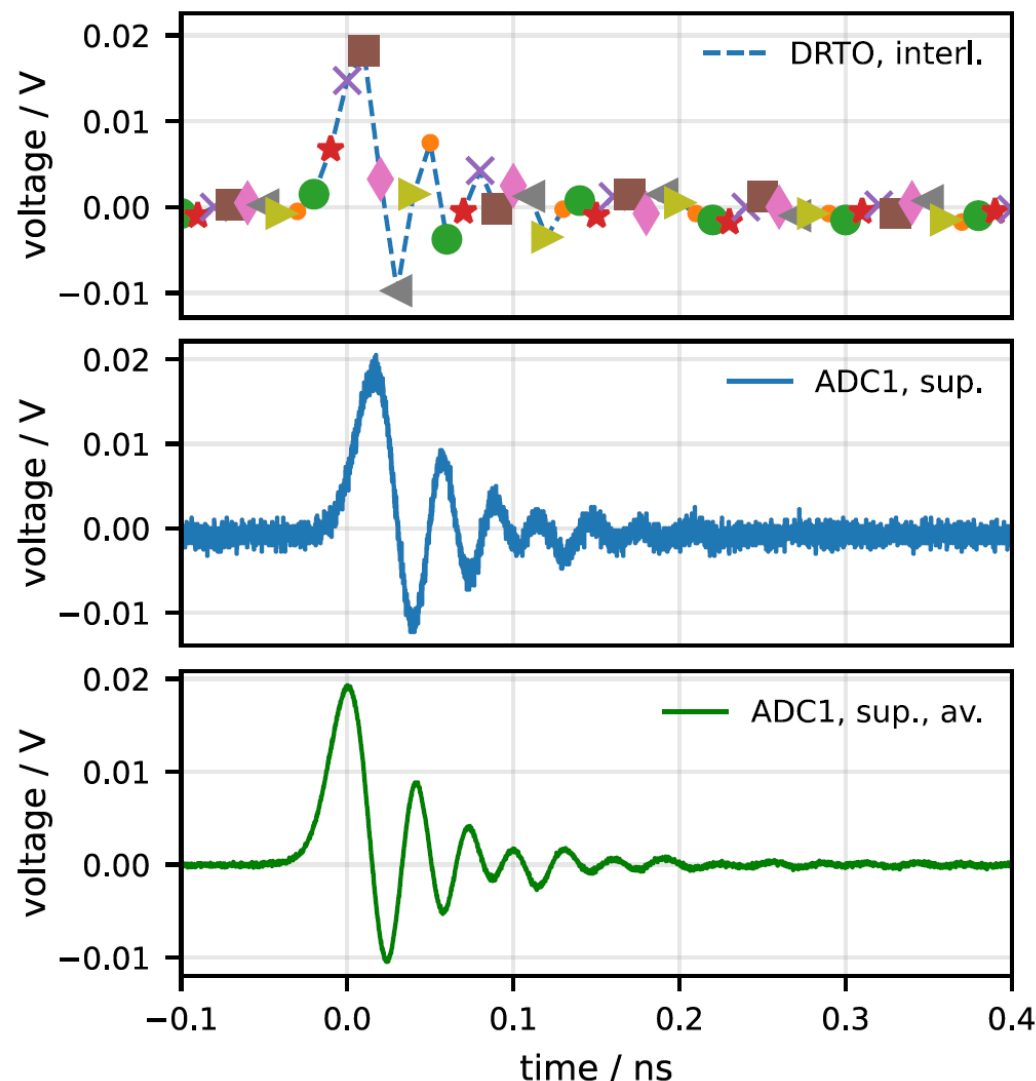
Absolute Transfer Functions

Setup



Main steps

- Port 1: fast pulse
Port 3: reference sine
- Separate data by sub-ADCs
- Superimpose and average data for each sub-ADC
- Calculate complex transfer functions using reference pulse data



Challenges:

- Pulse amplitude is very low
- Small dynamic range, high noise floor
- Align calibration data from photodiode to DRT0 data

Sequence Matching

Why do we need the reference signal?

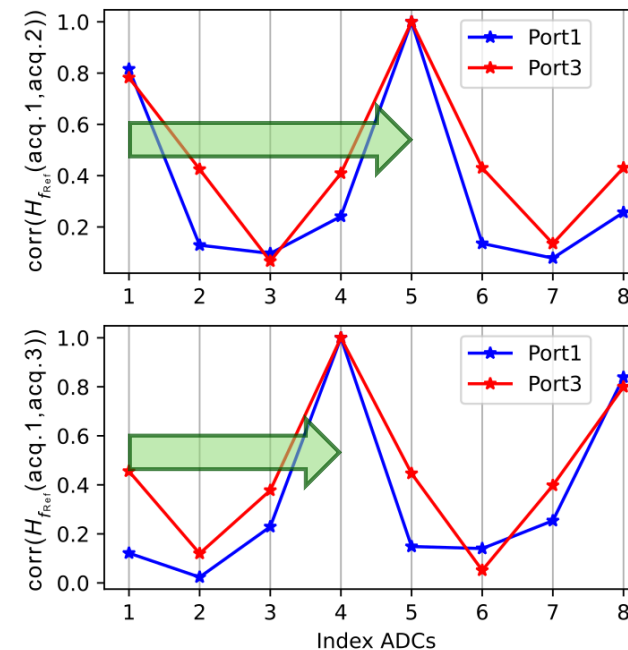
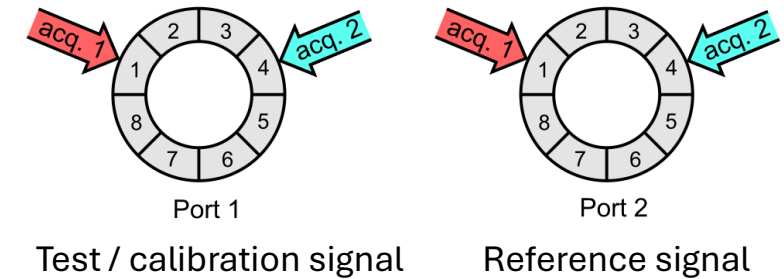
Problem:

- Each DRTO acquisition starts with a random sub-ADC
- How to apply the (relative) transfer functions to correct the signal?

Solution:

- Use reference signal at second port
- Evaluate relative transfer functions at f_{Ref}
- Correlate transfer functions to find shift
- Assumption: shift between ports remains constant between measurements

Example: cyclic use of 8 sub-ADCs, random starting ADC



Observation:

- Equal shift for both ports
- Reference signal can be used to find starting ADC of test signal

Result:

acq.2 starts with ADC 5
acq.3 starts with ADC 4

DRT0 Next Steps

- Investigate **combination** of methods: relative and absolute transfer functions
- Use **DRT0 model** to validate waveform correction and reconstruction algorithms for different instruments and signals
- Provide model and use cases in **online platform** to enable uptake

Acknowledgement

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- Grant number: 23NRM01 SBS Uncert

The logo for the Metrology Partnership, with 'METROLOGY' in blue above 'PARTNERSHIP' in blue.

Questions?



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